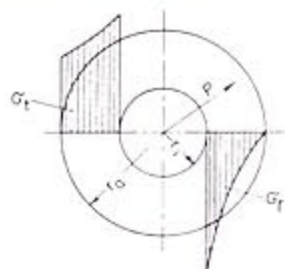


HUB CALCULATION

Thick wall cylinders and tubings may be calculated in accordance with an equation by Lamé.



$$\sigma_t = p \cdot \frac{r_i^2}{r_a^2 - r_i^2} \left(1 + \frac{r_a^2}{r^2} \right)$$

$$\sigma_r = p \cdot \frac{r_i^2}{r_a^2 - r_i^2} \left(1 - \frac{r_a^2}{r^2} \right)$$

From these, the following equations are derived for the hub calculation:

$$(1) \sigma_{tiN} \approx p_N \frac{(a_N^2 + 1)}{a_N^2 - 1} \quad \text{u.} \quad (2) \sigma_{raN} \approx \frac{2p_N \cdot C}{a_N^2 - 1}$$

Legend:

$$a_N = \frac{D_N}{D} \quad \begin{array}{l} \text{outer hub diameter} \\ \text{bore diameter} \end{array}$$

C = constant, depending on hub width

For full hub section over the width of the locking assembly

$$C = 0.6 \quad \text{if hub width } B \geq 2 L_1$$

$$C = 0.8 \quad \text{when using several locking assemblies, with } B \geq L_3(1+n); n = \text{number of l. ass.}$$

$$C = 1.0 \quad \text{for } B \geq L_1$$

As $\sigma_{tiN} > \sigma_{raN}$, equation (1) will be used for the calculation. Solved for D_N

$$D_N \approx D \cdot \sqrt{\frac{\sigma_{tiN} + p_N \cdot C}{\sigma_{tiN} - p_N \cdot C}} \quad \begin{array}{l} \text{as } \sigma_{tiN} \text{ should be } \leq \sigma_S \\ \text{using } \sigma_S = \sigma_{0.2}: \end{array}$$

$$D_N \geq D \cdot \sqrt{\frac{\sigma_{0.2N} + p_N \cdot C}{\sigma_{0.2N} - p_N \cdot C}}$$

If the hub is weakened (e. g. bores or threads), the hub diameter should be enlarged correspondingly (e. g. by the bore diameter)

For hollow shafts the equation is:

$$d_B \leq d \cdot \sqrt{\frac{\sigma_{0.2w} - 2p_w \cdot C}{\sigma_{0.2w}}}$$

General application:

Hollow shaft longer than $2 L_1$,

i. e.: C = 0.6

d_B = internal diameter of hollow shaft

Example:

A hub made of GS-52 with a width of $B \geq 2 L_1$ to be connected with a shaft $d = 100$ mm diameter by means of locking assembly TAS 3020

$$\text{GS-52} \rightarrow \sigma_{0.2} \approx 250 \text{ N/mm}^2$$

$$B \geq 2 L_1 \text{ corresponds to } C = 0.6$$

Shaft diameter $d = 100$ mm requires a locking assembly 100 x 145; therefore

$$D = 145 \text{ mm} \quad p_N \approx 157 \text{ N/mm}^2$$

$$D_N \geq 145 \sqrt{\frac{250 + 157 \cdot 0.6}{250 - 157 \cdot 0.6}} \geq 215.5$$

i. e. $D_N = 220 \text{ mm}$